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非线性大阻尼系统的摄动法

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摘要: 提出大阻尼非线性振动系统一种改进的摄动法, 并应用这种新的方法研究了大阻尼 Vanderpol 方程的一次近似解.

关键词: 非线性; 递推公式; 平均频率

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0 引言

在工程中, 有许多振动系统其阻尼都比较大, 而以前非线性振动理论中的摄动法只适合于小阻尼 $n = o(\epsilon)$ 的情况, 对于大阻尼 $n = o(1)$ 的情况并不适用. 本文采用新的解析方法对大阻尼情况进行了有效的处理, 得到了满意的结果. 在理论上比较严谨, 同时又有较高的计算精度.

1 周期解的构造及其递推公式

考虑系统

$$\ddot{x} + 2n\dot{x} + \omega^2 x = f(x, \dot{x}, t) + g(t) \quad (1)$$

对式(1)构造如下摄动解:

$$x = a \cos \varphi + u(t) + \epsilon_1 x_1(a, t) + \epsilon^2 x_2(a, t) + \dots$$

$$\frac{da}{dt} = -NA + \epsilon_1 A_1(a, t) + \epsilon^2 A_2(a, t) + \dots$$

$$\frac{d\varphi}{dt} = \omega^* + \epsilon_1 B_1(a, \varphi, t) + \epsilon^2 B_2(a, \varphi, t) + \dots \quad (2)$$

式中: $\omega^* = \sqrt{\omega^2 - n^2}$

$u(t)$ 为 $\ddot{x} + 2n\dot{x} + \omega^2 x = g(x)$ 的特解, 将 x, \dot{x}, x 代入式(1), 且把 $f(x, \dot{x}, t)$ 展开为 ϵ 幂级数, 最后

比较两端 ϵ'' 的系数得:

$$\begin{aligned} & (-na \frac{\partial A_n}{\partial a} + nA_n - 2a\omega^* + \frac{\partial A_n}{\partial t}) \cos \varphi - (2\omega^* A_n \\ & - 2naB_n - na^2 \frac{\partial B_n}{\partial a} + a\omega^* \frac{\partial B_n}{\partial \varphi} - \frac{\partial B_n}{\partial t}) \sin \varphi + (n^2 a^2 \\ & \frac{\partial^2 x_n}{\partial a^2} - n^2 a \frac{\partial x_n}{\partial a} + \omega x_n - \frac{\partial^2 x_n}{\partial t^2} - 2na \frac{\partial^2 x}{\partial a \partial t} + 2n \frac{\partial x_n}{\partial t}) = \\ & F_n(x_1 \dots x_{n-1}, A_1 \dots A_{n-1}, B_1 \dots B_{n-1}, t) \end{aligned} \quad (3)$$

$$\text{如: } F_n = C_0(a, t) + \sum_{m=1}^{k+1} [C_m(a, t) \cos m\varphi + \alpha_m(a, t) \sin m\varphi] \quad (4)$$

$$\text{令: } B_n(a, \varphi, t) = \alpha_0(a, t) + 2 \sum_{m=1}^k [\alpha_m(a, t) \cos m\varphi + \beta_m(a, t) \sin m\varphi] \quad (5)$$

将 F_n, B_n 代入式(3), 并令两端自由项、 $\cos m\varphi, \sin m\varphi$ 的系数相等, 于是得到确定 x_n, A_n, B_n 展开式中诸系数的递推公式如下:

$$\begin{aligned} & n^2 a^2 \frac{\partial^2 x_n}{\partial a^2} - n^2 a + \omega^* x_n + \frac{\partial}{\partial t} (\frac{\partial x_n}{\partial t} - 2na \frac{\partial x_n}{\partial a} + \\ & 2nx_n) \\ & = C_0 - na^2 \frac{\partial \beta_1}{\partial a} + a\omega^* \alpha_1 + a \frac{\partial \beta_1}{\partial t} \\ & - na \frac{\partial A_n}{\partial a} + nA_n - a\omega^* (2\alpha_0) + \frac{\partial A_n}{\partial t} = C_1 - na^2 \frac{\partial \beta_2}{\partial a} + a \frac{\partial \beta_2}{\partial t} \\ & na^2 \frac{\partial \alpha_0}{\partial a} - \omega^* (2A_n) - a \frac{\partial \alpha_0}{\partial t} = \alpha_1 + na^2 \frac{\partial \alpha_2}{\partial a} - a \frac{\partial \alpha_2}{\partial t} \end{aligned} \quad \left. \vphantom{\begin{aligned} & n^2 a^2 \frac{\partial^2 x_n}{\partial a^2} - n^2 a + \omega^* x_n + \frac{\partial}{\partial t} (\frac{\partial x_n}{\partial t} - 2na \frac{\partial x_n}{\partial a} + \\ & 2nx_n) \\ & = C_0 - na^2 \frac{\partial \beta_1}{\partial a} + a\omega^* \alpha_1 + a \frac{\partial \beta_1}{\partial t} \\ & - na \frac{\partial A_n}{\partial a} + nA_n - a\omega^* (2\alpha_0) + \frac{\partial A_n}{\partial t} = C_1 - na^2 \frac{\partial \beta_2}{\partial a} + a \frac{\partial \beta_2}{\partial t} \\ & na^2 \frac{\partial \alpha_0}{\partial a} - \omega^* (2A_n) - a \frac{\partial \alpha_0}{\partial t} = \alpha_1 + na^2 \frac{\partial \alpha_2}{\partial a} - a \frac{\partial \alpha_2}{\partial t} \end{aligned}} \right\}$$

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$$\left. \begin{aligned} -na^2 \frac{\partial \alpha_1}{\partial a} - a\omega^*(3\alpha_1) + a \frac{\partial \beta_1}{\partial a} = C_2 - na^2 \frac{\partial \beta_3}{\partial a} - a\omega^* \alpha_3 + a \frac{\partial \beta_3}{\partial a} \\ na^2 \frac{\partial \alpha_1}{\partial a} - \omega^*(3\beta_1) - a \frac{\partial \alpha_1}{\partial a} = \alpha_2 + na^2 \frac{\partial \alpha_3}{\partial a} - a\omega^* \beta_3 - a \frac{\partial \alpha_3}{\partial a} \\ \dots\dots\dots \\ -na^2 \frac{\partial \alpha_{m-1}}{\partial a} - a\omega^*(m+1)\alpha_{m-1} + a \frac{\partial \beta_{m-1}}{\partial a} = C_m - na^2 \frac{\partial \beta_{m+1}}{\partial a} \\ -a\omega^*(m-1)\alpha_{m+1} + a \frac{\partial \beta_{m+1}}{\partial a} \\ na^2 \frac{\partial \alpha_{m-1}}{\partial a} - a\omega^*(m+1)\beta_{m-1} - a \frac{\partial \alpha_{m-1}}{\partial a} = d_m + na^2 \frac{\partial \alpha_{m+1}}{\partial a} \\ -a\omega^*(m-1)\beta_{m+1} - a \frac{\partial \alpha_{m+1}}{\partial a} \\ m=3, 4, \dots, k-1 \\ -na^2 \frac{\partial \alpha_{k-1}}{\partial a} - a\omega^*(k+1)\alpha_{k-1} + a \frac{\partial \beta_{k-1}}{\partial a} = C_k \\ na^2 \frac{\partial \alpha_{k-1}}{\partial a} - a\omega^*(k+1)\beta_{k+1} - a^2 \frac{\partial \alpha_{k-1}}{\partial a} = d_k \\ -na^2 \frac{\partial \beta_k}{\partial a} - a\omega^*(k+2)\alpha_k + a \frac{\partial \beta_k}{\partial a} = C_{k+1} \\ na^2 \frac{\partial \alpha_k}{\partial a} - a\omega^*(k+2)\beta_{k+1} - a \frac{\partial \alpha_k}{\partial a} = d_{k+1} \end{aligned} \right\} (6)$$

当式(6)右端为 a 的多项式,且其系数为 t 的函数时,易验证:对应于 a^l 项,如

$$d_{k+1} = d_{k+1}^{(l)}(t) a^l, c_{k+1} = c_{k+1}^{(l)}(t) a^l$$

有与之相应的特解有

$$\alpha_k = \alpha_k^{(l)}(t) a^{l-1}, \beta_k = \beta_k^{(l)}(t) a^{l-1}$$

由于上述诸式可化为一线性微分方程组,故它们对应于整个多项式之通解可由对应于每一项之特解的叠加求出.在求得 α_k 与 β_k 后,按照式(6)自下而上顺序可依次将

$$\alpha_{k-1}, \beta_{k-1}, \dots, \alpha_1, \beta_1, \alpha_0, A_n \text{ 及 } x_n \text{ 求出.}$$

2 大阻尼 Vanderpol 方程的一次近似解

研究受简谐干扰力的大阻尼 Vanderpol 方程:

$$\ddot{x} + 2n\dot{x} + \omega^2 x = \epsilon(1-x^2)\dot{x} + Hsm(\nu t + q) \quad (7)$$

此时: $F_1 = (1-x^2) = [1 - (a \cos \varphi + hsm\nu t)^2]$

$$(-ncos\varphi - a\omega^* sm\varphi + h\nu \cos \nu t)$$

$$= c_0(a, t) + \sum_{m=1}^3 [c_m(a, t) \cos m\varphi + d_m(a, t)$$

$$smm\varphi] \text{ 式中: } c_0(a, t) = (\nu - \frac{1}{4} \nu h^3 - \frac{1}{2} a\nu h a^2) \cos \nu t + nha^2 \sin \nu t + \frac{1}{4} \nu h^3 \cos \nu t$$

$$c_1(a, t) = (\frac{1}{2} h^2 - 1) na + \frac{3}{4} na^3 - \frac{1}{2} nh^2 a \cos \nu t$$

$$- \nu h^2 a \sin 2\nu t$$

$$d_1(a, t) = (\frac{1}{2} h^2 - 1) \omega^* a - \frac{1}{4} \omega^* a^3 - \frac{1}{2} \omega^* h^2 a \cos 2\nu t$$

$$c_2(a, t) = -\frac{1}{2} \nu h a^2 \sin \nu t$$

$$d_2(a, t) = \omega^* h a^2 \sin \nu t$$

$$c_3(a, t) = \frac{1}{4} na^3$$

$$d_3(a, t) = \frac{1}{4} \omega^* a^3 \quad (8)$$

而 $B_1(a, \varphi, t) = \alpha_0(a, t) + 2 \sum_{m=1}^2 [\alpha_m(a, t) \cos m\varphi + \beta_m(a, t) \sin m\varphi]$

首先研究非共振情况,此时 $\nu \neq \omega^*$, 可得:

$$\alpha_0(a, t) = \frac{n}{2\omega^*} (1 - \frac{n^2}{2}) - \frac{n\omega^* (5\omega^{*2} + 2n^2)}{4(\omega^{*2} + n^2)(4\omega^{*2} + n^2)} a^2 + \frac{\omega^* h^2}{4\omega^{*2} + n^2} a^2 + \frac{\omega^* h^2}{4\omega^{*2} + n^2} (N \cos 2\nu t + \nu \sin 2\nu t)$$

$$\alpha_1(a, t) = \frac{h\omega^* h^2}{\Delta} [3m\nu(\omega^{*2} + n^2 + \nu^2) \cos \nu t + (-54\omega^{*4} - 2n^4 - \nu^4 - 24\omega^{*2}n^2 + 9\omega^{*2}\nu^2) \sin \nu t]$$

$$\alpha_2(a, t) = -\frac{n\omega^*}{4(4\omega^{*2} + n^2)} a^2$$

$$\beta_2(a, t) = -\frac{2\omega^{*2} + n^2}{4(4\omega^{*2} + n^2)} a^2$$

$$A_1(a, t) = \frac{1}{2} (1 - h^2) a - \frac{2\omega^{*4} + 7\omega^{*2}n^2 + 2n^4}{4(\omega^{*2} + n^2)(4\omega^{*2} + n^2)} a^3 + \frac{h^2}{4\omega^{*2} + n^2} [(\omega^{*2} - \nu^2) \cos 2\nu t + \nu \sin 2\nu t] a$$

$$x_1(a, t) = \frac{\nu h(1 - \frac{h^2}{2})}{(\omega^{*2} - \nu^2)^2 + 4n^4} [(\omega^{*2} - \nu^2) \cos \nu t + 2n \sin \nu t] + \frac{(u_1 \cos \nu t + u_2 \sin \nu t) a^2}{4[(\omega^{*2} - 9\nu^2) + 36n^4]} [\omega^{*2} - 9\nu^2 \cos 3\nu t + 6n \sin 3\nu t] \quad (9)$$

式中: $\Delta = (9\omega^{*2} - \nu^2)^2 + n^2(18\omega^{*2} + n^2 + 2\nu^2)$

$$u_1 = \frac{1}{2} \frac{1}{(\omega^{*2} - \nu^2)^2 + 4n^4} [(\omega^{*2} - \nu^2)(-\nu h + n p_1 + \nu p_2 + \omega^* q_1) + 2n(2nh - \nu p_1 - n p_2 + \omega^* Q_2)]$$

$$u_2 = \frac{1}{2} \frac{1}{(\omega^{*2} - \nu^2)^2 + 4n^4} [(\omega^{*2} - \nu^2)(2nh - \nu p_1 - \nu p_2 + \omega^* q_2) - 2n(-\nu h + n p_1 - n p_2 + \omega^* Q_1)]$$

$$p_1 = -\frac{3hn\nu}{\Delta} (\omega^{*2} + n^2 + \nu^2)$$

$$p_2 = \frac{h}{\Delta} (-54\omega^{*4} - 2n^4 - v^4 - 24\omega^{*2}n^2 + 9\omega^{*2}v^2 - 3n^2v^2)$$

$$q_1 = -\frac{3h\omega^*v}{\Delta} (9\omega^{*2} + n^2 + v^2)$$

$$q_2 = -\frac{h\omega^*}{\Delta} (-36\omega^{*2}n + n^2v - v^3) \quad (10)$$

令 $\frac{da}{dt} = 0$ 可得到系统的周期解

$$a^* = 2 \left[\frac{4\omega^4 - 3n^4}{2\omega^2 + 3\omega n - 3n^2} \left(\frac{1}{2} - \frac{h^2}{2} - \frac{n}{\epsilon} \right) \right]^{\frac{1}{2}} \quad (11)$$

在实际工程中一般有 $\omega > n$, 由此可见:

① $\frac{1}{2} - \frac{h^2}{2} - \frac{n}{\epsilon} > 0$ 时, a^* 为实数值, 这表明式

(7) 除有一圆频率为 v 的周期解 $h \sin \psi$ 之外, 尚有一周期解 $a^* \cos \varphi + \epsilon x_1(a, t)$, 它的平均频率为

$\omega^* + \epsilon a^*$ 此时有

$$\alpha_0 = \frac{n}{2\omega^*} \left(1 - \frac{h^2}{2} \right) - \frac{n\omega^* (5\omega^{*2} + 2n^2)}{4(\omega^{*2} + n^2)(4\omega^{*2} + n^2)}$$

a^*

还可求得

$$\frac{dA_1}{da^*} = -\frac{2\omega^{*4} + 2\omega^{*2}n^2}{2(\omega^{*2} + n^2)(4\omega^{*2} + n^2)} a^{*2} < 0$$

故上述周期解

$a^* \cos \varphi + \epsilon x_1(a, t)$ 是稳定的.

② 当 $\frac{1}{2} - \frac{h^2}{4} - \frac{n}{\epsilon} \rightarrow 0$ 时 $a^* \rightarrow 0$

周期解 $a^* \cos \varphi + \epsilon x_1(a, t)$ 消失.

③ 当 $\frac{1}{2} - \frac{h^2}{4} - \frac{n}{\epsilon} < 0$ 时

a^* 是虚数, 这表明周期解 $a^* \cos \varphi + \epsilon x_1(a, t)$

不存在, 系统(7)最后只依 $x = h \sin \psi$ 作强迫振动.

其次研究其振情况, $v = \omega^*$

为使系统不出现永年项, 设 $H = \epsilon H^*$, 又为计算简单设激励力初位相 $\theta = 0$, 此外设 $\omega^* = v - \epsilon \sigma$, σ 为解谐参数, 于是式(7)代为

$$\ddot{x} + 2\dot{N}\dot{x} + (v^2 + n^2)x = \epsilon[(1-x^2)\dot{x} + 2\sigma x + H^* \sin \psi] \quad (12)$$

设 $x = a \cos(\psi + \phi) + \epsilon x_1(a, t)$

$$\frac{da}{dt} = -na + \epsilon A_1(a, t)$$

$$\frac{d\phi}{dt} = \epsilon B_1(a, \phi, t)$$

令 $\varphi = \psi + \phi$ 则此时

$$F_1(1-x^2)\dot{x} + 2\sigma x + H^* \sin \psi$$

$$= [-F^* \sin \varphi + (2\sigma - n)a + \frac{3}{4}na^3] \cos \varphi +$$

$$(F^* \cos \varphi - va + \frac{1}{4}na^3) \sin \varphi + \frac{1}{4}na^3 \cos^3 \varphi + \frac{1}{4}$$

$$va^3 \sin^3 \varphi$$

按照上面的方法可得

$$\frac{da}{dt} = A(a, \phi); \quad \frac{d\phi}{dt} = B(a, \phi)$$

为得定常解令:

$$\frac{da}{dt} = A(a, \phi) = 0 \quad \frac{d\phi}{dt} = B(a, \phi) = 0$$

如上式有稳定奇点 (a^*, ϕ^*) 时,

式(12)将有一稳定周期解

$$x = a^* \cos(\psi + \phi^*)$$

3 结论

综上所述, 可见本文提出的改正摄动法, 对解决大阻尼非线性系统实际问题是较为有效的可行的方法.

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The Perturbation Method of Non-linear and Great-damping Vibration System

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Abstract: In this article, a new improved interference method about great-damping and non-linear vibration systems is put forward and applied to research the approximate root of Vanderpol equation.

Key words: non-linear; recurrence formula; mean frequency